


<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Brief			
	Job Number : F0021	By : anw	Date:Feb 02	
	Document No : 007B	Checked : jjg	Date:Feb 02	

**Brief**

The brief is to prepare calculated values for the capacity of a ladder beam to BS 8118.

The beams are fabricated from tube extrusions in aluminium alloy 6082 T6

The geometry of the beam is as shown on drawing No F0021/009

The beams have been tested and the results are compared in the summary


**Material**

The alloy 6082T6 has the following properties

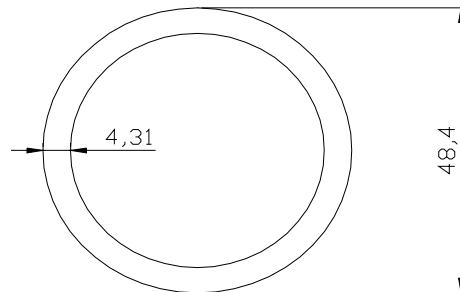
$\rho_0 = 255 \text{ N/mm}^2$

$\rho_a = 280 \text{ N/mm}^2$


$\rho_v = 155 \text{ N/mm}^2$

CALCULATION SHEET	Project : Apollo aluminium ladder beam			
	Element : Section Properties			
	Job Number : F0006	By : anw	Date:Feb 02	
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**Main boom and verticals**



Area:	596.99 mm <sup>2</sup>
Bounding box:	X: -24.2 -- 24.2 mm Y: -24.2 -- 24.2 mm
Moments of inertia:	X: 146449.49 mm <sup>4</sup> Y: 146449.49 mm <sup>4</sup>
Radii of gyration:	X: 15.66 mm Y: 15.66 mm
Elastic Modulus	X: 6051.63 mm <sup>3</sup> Y: 6051.63 mm <sup>3</sup>
Plastic Modulus	X: 8169.70 mm <sup>3</sup> Y: 8169.70 mm <sup>3</sup>

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Main boom			
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### Classification

Slenderness

$$\begin{aligned}\beta &= 3*((D/t)^{0.5}) \\ &= 3*((48.4-4.31)/4.31)^{0.5} \\ &= 9.595169899\end{aligned}$$

$$\begin{aligned}\varepsilon &= (250/p_0)^{0.5} \\ &= (250/255)^{0.5} \\ &= 0.99\end{aligned}$$

$$\begin{aligned}\beta_1 &= 15\varepsilon \\ &= 15*0.99 \\ &= 14.85 \\ &> 9.6\end{aligned}$$

**Section is compact**

**Bending capacity** 4.5.2.2

$$\begin{aligned}M_{rs} &= p_0 S_n / \gamma_m & p_0 &= 255 \text{ N/mm}^2 \\ & & S_n &= 8.17 \text{ cm}^3 \\ & & \gamma_m &= 1.2 \\ &= 255 * 8.17 / 1200 \\ &= \mathbf{1.74 \text{ kNm}}\end{aligned}$$

**Shear** 4.5.3.2

$$\begin{aligned}V_{rs} &= p_v A_v / \gamma_m & p_v &= 155 \text{ N/mm}^2 \\ & & A_v &= 0.6A \\ & & &= 0.6 * 597 \\ & & &= 358.2 \text{ mm}^2 \\ & & \gamma_m &= 1.2 \\ &= 155 * 358.2 / 1200 \\ &= \mathbf{46.27 \text{ kN}}\end{aligned}$$

### Lateral Torsional Buckling

No check required for CHS


**Tension**

4.6  
for General Tension

$$\begin{aligned}P_{rs} &= p_0 A / \gamma_m & p_0 &= 255 \text{ N/mm}^2 \\ & & A &= 597 \text{ mm}^2 \\ & & \gamma_m &= 1.3 \\ &= 255 * 597 / 1300 \\ &= \mathbf{117.10 \text{ kN}}\end{aligned}$$

For local at splice

$$\begin{aligned}P_{rs} &= p_a A_n / \gamma_m & p_a &= 280 \text{ N/mm}^2 \\ & & A_n &= A - 2dt \\ & & &= 597 - 2 * 14 * 4.31 \\ & & &= 476.32 \text{ mm}^2 \\ & & \gamma_m &= 1.3 \\ &= 280 * 476.3 / 1300 \\ &= \mathbf{102.59 \text{ kN}}\end{aligned}$$

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**Compression**

**4.7**

$$Pr = \frac{psA}{\gamma_m}$$

**for 1m bracing**

$$L = 950.00 \text{ m}$$

$$r = 15.66 \text{ mm}$$

$$\lambda = \frac{KL}{r} \quad K = 0.7$$

$$= \frac{0.7 \cdot 950}{15.66}$$

$$= 42.46$$

**Fig 4.10b gives**


$$ps = 180.00 \text{ N/mm}^2$$

$$A = 597 \text{ mm}^2$$

$$\gamma_m = 1.2$$

$$Pr = \frac{180 \cdot 597}{1200}$$

$$= 89.55 \text{ kN}$$

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Verticals			
	Job Number : F0006	By : anw	Date:Feb 02	
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### Classification

Slenderness

$$\begin{aligned}\beta &= 3*((D/t)^{0.5}) \\ &= 3*((48.4-4.31)/4.31)^{0.5} \\ &= 9.595169899\end{aligned}$$

$$\begin{aligned}\epsilon &= (250/p_0)^{0.5} \\ &= (250/255)^{0.5} \\ &= 0.99\end{aligned}$$

$$\begin{aligned}\beta_1 &= 15\epsilon \\ &= 15*0.99 \\ &= 14.85 \\ &> 9.6\end{aligned}$$

**Section is compact**

**Bending capacity** 4.5.2.2

$$\begin{aligned}M_{rs} &= p_0 S_n / \gamma_m && p_0 = 255 \text{ N/mm}^2 \\ & && S_n = 8.17 \text{ cm}^3 \\ & && \gamma_m = 1.2 \\ &= 255 * 8.17 / 1200 \\ &= \mathbf{1.74 \text{ kNm}}\end{aligned}$$

**Shear** 4.5.3.2

$$\begin{aligned}V_{rs} &= p_v A_v / \gamma_m && p_v = 155 \text{ N/mm}^2 \\ & && A_v = 0.6A \\ & && = 0.6 * 597 \\ & && = 358.2 \text{ mm}^2 \\ & && \gamma_m = 1.2 \\ &= 155 * 358.2 / 1200 \\ &= \mathbf{46.27 \text{ kN}}\end{aligned}$$

### Lateral Torsional Buckling

No check required for CHS


**Tension**

4.6  
for General Tension

$$\begin{aligned}P_{rs} &= p_0 A / \gamma_m && p_0 = 255 \text{ N/mm}^2 \\ & && A = 597 \text{ mm}^2 \\ & && \gamma_m = 1.3 \\ &= 255 * 597 / 1300 \\ &= \mathbf{117.10 \text{ kN}}\end{aligned}$$

For local at splice

$$\begin{aligned}P_{rs} &= p_a A_n / \gamma_m && p_a = 280 \text{ N/mm}^2 \\ & && A_n = A - 2dt \\ & && = 597 - 2 * 14 * 4.31 \\ & && = 476.32 \text{ mm}^2 \\ & && \gamma_m = 1.3 \\ &= 280 * 476.3 / 1300 \\ &= \mathbf{102.59 \text{ kN}}\end{aligned}$$

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Verticals			
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**Compression**

**4.7**

$$Pr = \frac{psA}{\gamma_m}$$

$$L = 260.00 \text{ m}$$

$$r = 15.66 \text{ mm}$$

$$\lambda = \frac{KL}{r} \qquad K = 0.85$$

$$= \frac{0.85 \times 260}{15.66}$$

$$= 14.11$$

Fig 4.10b gives


$$ps = 250.00 \text{ N/mm}^2$$

$$A = 597 \text{ mm}^2$$

$$\gamma_m = 1.2$$

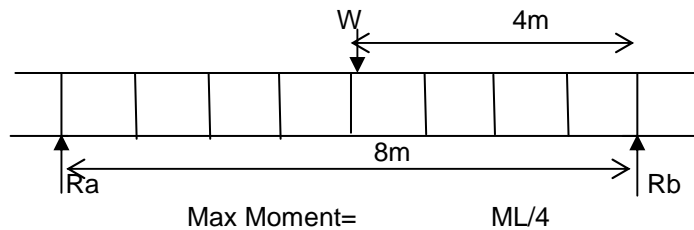
$$Pr = \frac{250 \times 597}{1200}$$

$$= 124.38 \text{ kN}$$

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Load Case 3- 1m bracing			
	Job Number : F0006	By : anw	Date:Feb 02	
	Document No : 007B	Checked : jgg	Date:Feb 02	

Load Case 2      Load at middle      (note Load case 1 was not used for analysis - self weight only)  
 10kN applied at centre

Element	Action	Formula	Ultimate	Calculated	Factor
Boom	Moment	Mrs	1.74	0.78	2.23
	Shear	Vrs	46.27	3.4	13.61
	Tension	Prs	117.10	81.2	1.44
	Compression	Pry	89.55	81.2	1.10
		coexist M		0.8	
	Combined	P/Prs+M/Mrs<1		1.37	0.73
Vertical	Moment	Mrs	1.74	1.01	1.72
	Shear	Vrs	46.27	6.6	7.01
	Tension	Prs	117.10	0.03	3903.46
	Compression	Pry	124.38	6.6	18.85
		coexist M		0	
	Combined	P/Prs+M/Mrs<1		0.05	18.85
Factor =					0.73



so for ultimate condition

$$W = \frac{1.33 \times 10}{1.33} = 13.30 \text{ kN}$$

apply factor from above

$$W_f = 13.3 \times 0.73 = 9.71$$


so maximum moment is as above

$$\begin{aligned} \text{Ultimate } M_u &= W_f \times 8/4 \\ &= 9.71 \times 8/4 \\ &= 19.42 \text{ kN} \end{aligned}$$

and for allowable value

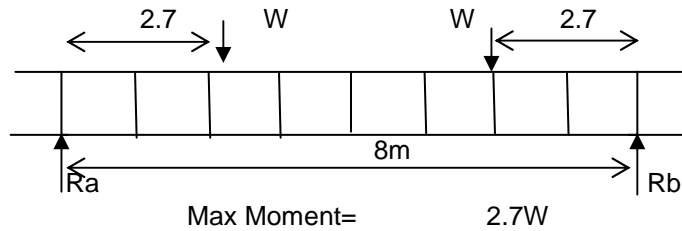
$$\begin{aligned} \text{allowable max moment} &= 19.42 / 1.33 \\ &= 14.60 \text{ kN} \end{aligned}$$

<b>Moment values</b>	<b>Ultimate</b>	<b>19.42 kN</b>
	<b>Allowable</b>	<b>14.60 kN</b>

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Load Case 4- 1m bracing			
	Job Number : F0006	By : anw	Date:Feb 02	
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Load Case 4      Load at third points  
 10kN applied at each of the two third points

Element	Action	Formula	Ultimate	Calculated	Factor
Boom	Moment	Mrs	1.74	3.32	0.52
	Shear	Vrs	46.27	0.19	243.53
	Tension	Prs	117.10	260.6	0.45
	Compression	Pry	89.55	260.6	0.34
		coexist M		0.45	
	Combined	P/Prs+M/Mrs<1		3.17	0.32
Vertical	Moment	Mrs	1.74	4.96	0.35
	Shear	Vrs	46.27	32.7	1.41
	Tension	Prs	117.10	0.06	1951.73
	Compression	Pry	124.38	16.3	7.63
		coexist M		0.021	
	Combined	P/Prs+M/Mrs<1		0.14	6.99
Factor =					0.32



so for ultimate condition

$$W = \frac{1.33 \cdot 10}{13.30} \text{ kN}$$

apply factor from above

$$W_f = \frac{13.3 \cdot 0.32}{4.21}$$


so maximum moment is as above

$$\begin{aligned} \text{Ultimate } M_u &= W_f \cdot 2.7 \\ &= 2.7 \cdot 4.21 \\ &= \mathbf{11.36 \text{ kNm}} \end{aligned}$$

and for allowable value

$$\begin{aligned} \text{allowable max moment} &= \frac{11.36}{1.33} \\ &= \mathbf{8.54 \text{ kNm}} \end{aligned}$$

<b>Moment values</b>	<b>Ultimate</b>	<b>11.36 kN</b>
	<b>Allowable</b>	<b>8.54 kN</b>

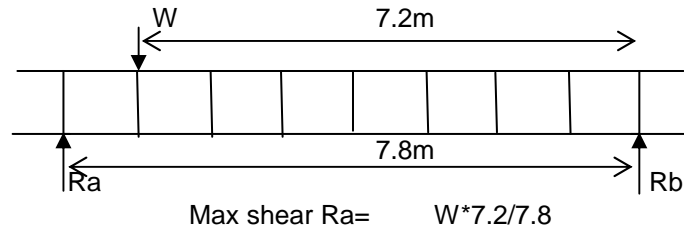
<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Load Case 2- 1m bracing			
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Load Case 4

Shear

10kN applied 0.6m from end

Element	Action	Formula	Ultimate	Calculated	Factor
Boom	Moment	Mrs	1.74	1.05	1.65
	Shear	Vrs	46.27	6.3	7.34
	Tension	Prs	117.10	22.9	5.11
	Compression	Pry	89.55	22.9	3.91
		coexist M		0.27	
	Combined	P/Prs+M/Mrs<1		0.41	2.43
Vertical	Moment	Mrs	1.74	1.6	1.09
	Shear	Vrs	46.27	10.5	4.41
	Tension	Prs	117.10	0.01	11710.38
	Compression	Pry	124.38	6.5	19.14
		coexist M		0.85	
	Combined	P/Prs+M/Mrs<1		0.54	1.85
				Factor =	1.09



so for ultimate condition

$$W = \frac{1.33 \cdot 10}{1.33} = 13.30 \text{ kN}$$

apply factor from above

$$W_f = 13.3 \cdot 1.09 = 14.43 \text{ kN}$$


so reaction at A is max shear

$$\begin{aligned} \text{Ultimate Ra} &= W_f \cdot 7.2 / 7.8 \\ \text{Ultimate shear} &= 13.32 \text{ kN} \end{aligned}$$

and for allowable value

$$\begin{aligned} \text{allowable Shear} &= 13.35 / 1.33 \\ &= 10.02 \text{ kN} \end{aligned}$$

<b>Shear values</b>	<b>Ultimate</b>	<b>13.32 kN</b>
	<b>Allowable</b>	<b>10.02 kN</b>

<b>CALCULATION SHEET</b>	Project : Apollo aluminium ladder beam			
	Element : Summary			
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### Test Results

The test results for mid point and third point moments are as shown  
These are based on the failure and yield values.

<b>Ultimate moment</b>	<b>14.9 kNm</b>
<b>Allowable moment</b>	<b>11.2 kNm</b>

Based on the deflection criteria of the Code then the values reduce to

<b>Ultimate moment</b>	<b>12.4 kNm</b>
<b>Allowable moment</b>	<b>9.3 kNm</b>

### Selected results

From calculated values confirmed by test results for bracing at 1m intervals

Max moment on the beam is

<b>Ultimate moment</b>	<b>11.36 kNm</b>
<b>Allowable moment</b>	<b>8.54 kNm</b>

and Maximum Shear is

<b>Ultimate shear</b>	<b>13.32 kN</b>
<b>Allowable shear</b>	<b>10.02 kN</b>

The calculated values are less than the tested values in this case due to the failure being related to the moments at the joints.

For simply supported ladder beam with a compression chord restraint at 1m intervals

Allowable Bending Moment	8.54 kNm
Allowable Shear	10.02 kN

Allowable loads for load distributions

Type of Load	Clear span (m)										
		3	4	5	6	7	8	9	10	11	12
Uniformly Distributed load	kN/m	6.7	4.3	2.7	1.9	1.4	1.1	0.8	0.7	0.6	0.5
Total UDL	kN	20.0	17.1	13.7	11.4	9.8	8.5	7.6	6.8	6.2	5.7
Single point load (mid Point)	kN	11.4	8.5	6.8	5.7	4.9	4.3	3.8	3.4	3.1	2.8
Two point loads (third points)	Each kN	8.5	6.4	5.1	4.3	3.7	3.2	2.8	2.6	2.3	2.1
Three point loads ( quarter points)	Each kN	5.7	4.3	3.4	2.8	2.4	2.1	1.9	1.7	1.6	1.4

Notes

1. Above allowable loads may be increased by 1.11 for **wind loading only**
2. This table is provided as a guide only and assume all loads are applied at restrained nodes. All scaffolds and structures should be checked by a qualified structural engineer.
3. Maximum capacity of a point load mid way between nodes is 15kN but overall buckling of the top chord should be checked if loads are placed other than at restrained loads.
4. Loads indicated in italics are limited by shear.